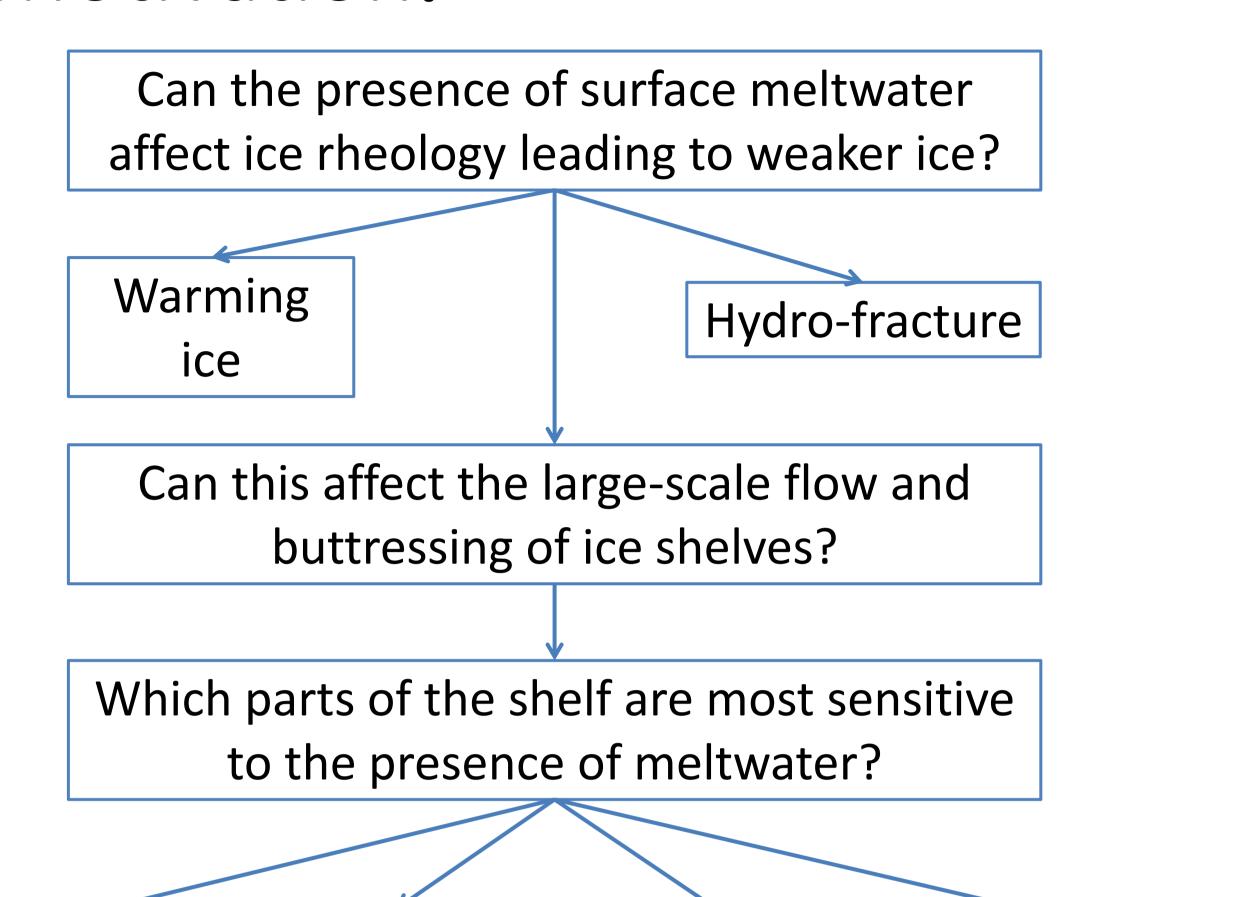
Martin Wearing (LDEO)

Motivation:



Margins

Pinning points

Grounding line

Elsewhere

Idealized Ice-Shelf Model:

- Parallel Channel
- Flow in along-channel (x) direction only. No-slip condition along sides.
- Uniform shelf-thickness across channel width

Force Balance
$$4\frac{\partial}{\partial x}\left(\mu H\frac{\partial u}{\partial x}\right) + \frac{\partial}{\partial y}\left(\mu H\frac{\partial u}{\partial y}\right) = \rho g'H\frac{\partial H}{\partial x}$$

Rheology
$$\mu = (1-D)B\varepsilon_{II}{}^{(1-n)/2n}$$

Evolve Thickness

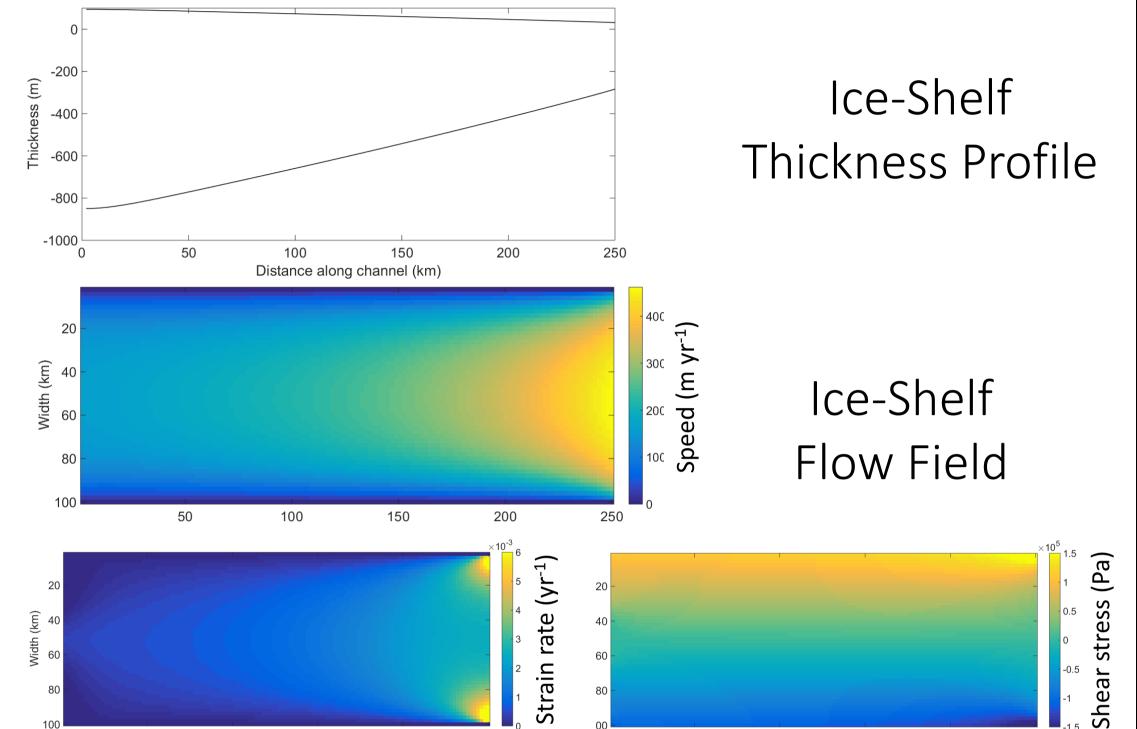
$$\frac{\partial H}{\partial t} + \nabla \cdot (Hu) = 0$$

- Vertical uniform rheology.
- Specify spatial variation in flow-law parameter B and damage D.
- Run to steady state
- Calculate vertically and horizontally integrated buttressing from shear stress

Lamont-Doherty Earth Observatory

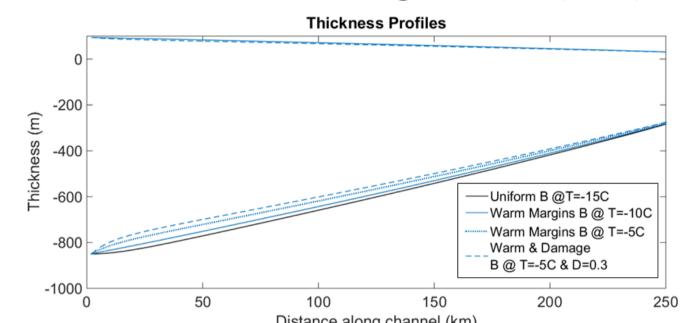
Base Case:

Ice shelf rheology uniform with no damage (D=0) and flow-law parameter B appropriate for at -15°C: $B(-15C) = 1.68 \times 10^8 \text{Pa s}^{1/3}$



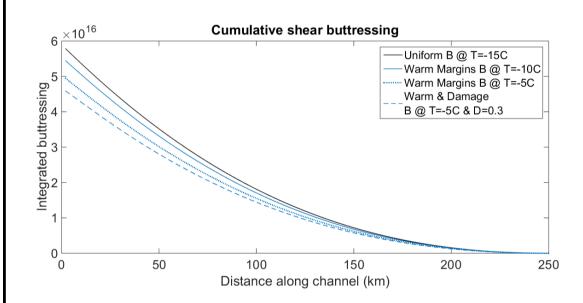
Margins: (within 6 km (3 grid points) of walls)

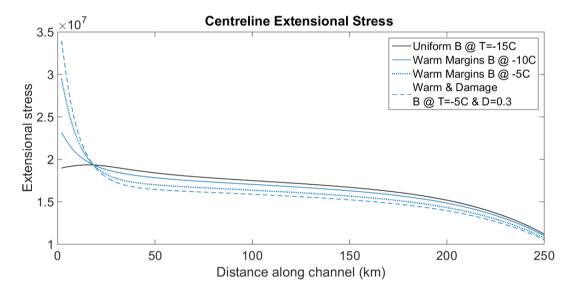
- Warm: *B*(-10C) & *B*(-5C)
- Warm and damage ice: B(-5C) with D=0.3



Horizontal and vertically integrated shear stress back from calving front.

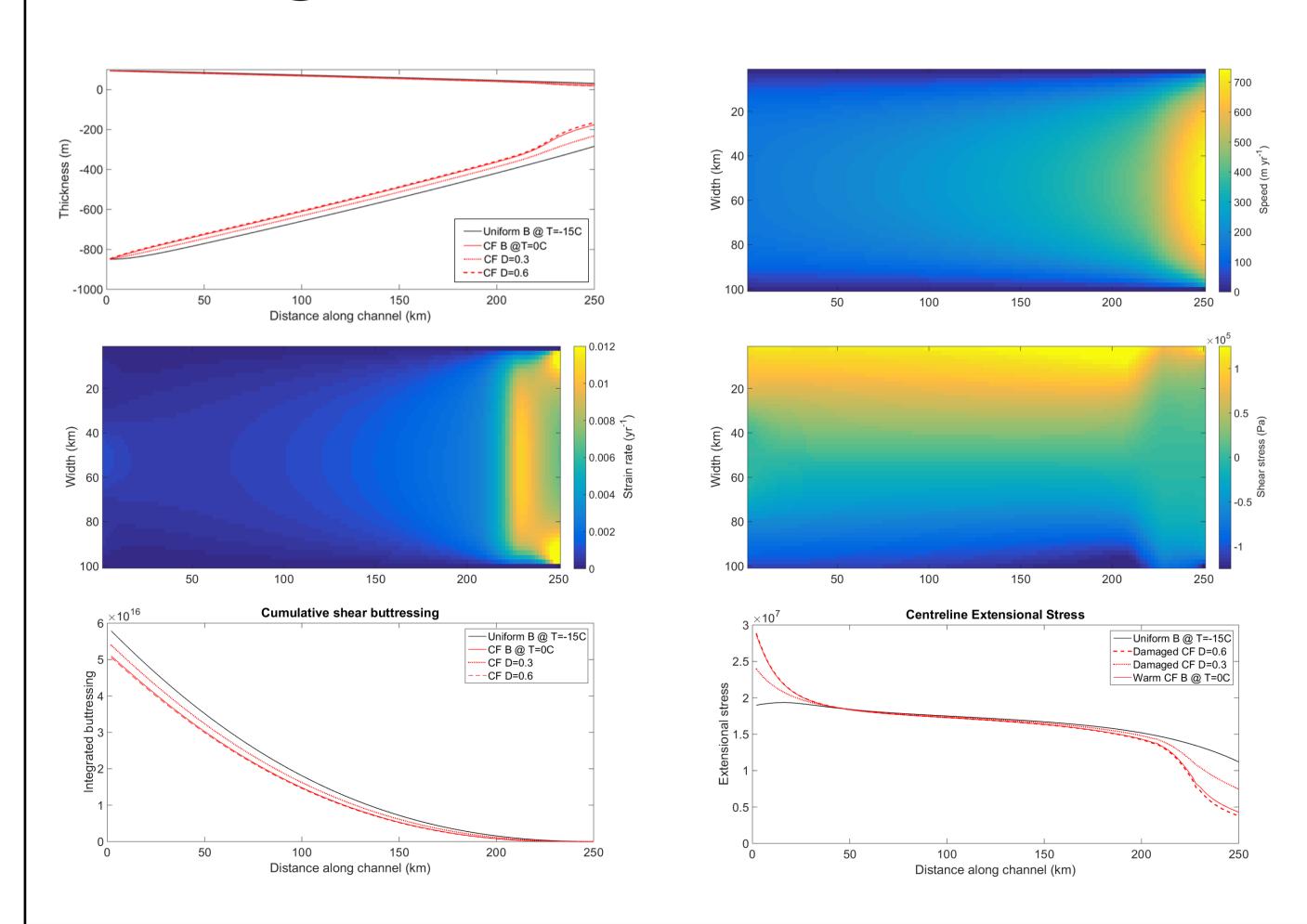
extensional stress along centreline.





Vertically integrated

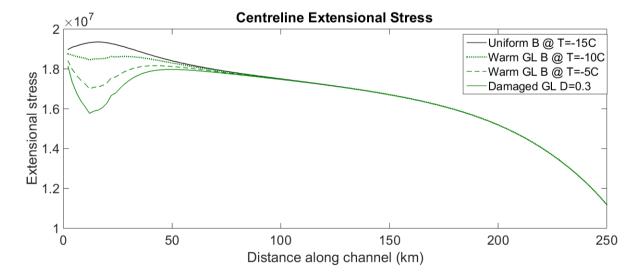
Calving front: Warm or damage final 30 km of shelf



Grounding Line (GL):

(Warm/damage 10 km downstream of GL)

Thickness profile and shear buttressing similar in all cases.



Findings:

In these simple experiments, warming or damaging the margins and calving front of the ice shelf had the biggest impact on large-scale flow. Confining this effect to the grounding line had least affect. However, this ice would advect into the whole shelf potentially leading to weakening

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